

# Cross interactions

## 1) Warning

Be careful, the calculations of the mass jacobian in this paper is outdated (but still valid, refer to the new paper: Return of the Jacobian)

## 2) Why?

One of our hypotheses is that the two active arms are completely decoupled. Our main reason behind it is that the revolute joints don't transfer load between them and that the high gear ratio "blocks" every (small) disturbance on the load shaft from reaching the motor shaft.

This is a good first approximation because it allows us to ignore every cross-interactions between the two servo motors and design the controllers independently.

We can apply a more rigorous approach in the study of these effects before moving forward with other tasks. (Just in case the professor wants to be pedantic).

## 3) 2-DOF Kinematics

Seen from the 2 load shafts our system has only masses and moments of inertia, no potential energies or dissipations.

$$T = \frac{1}{2} \dot{\underline{y}}^T [m_{ph}] \dot{\underline{y}} \quad 1.$$

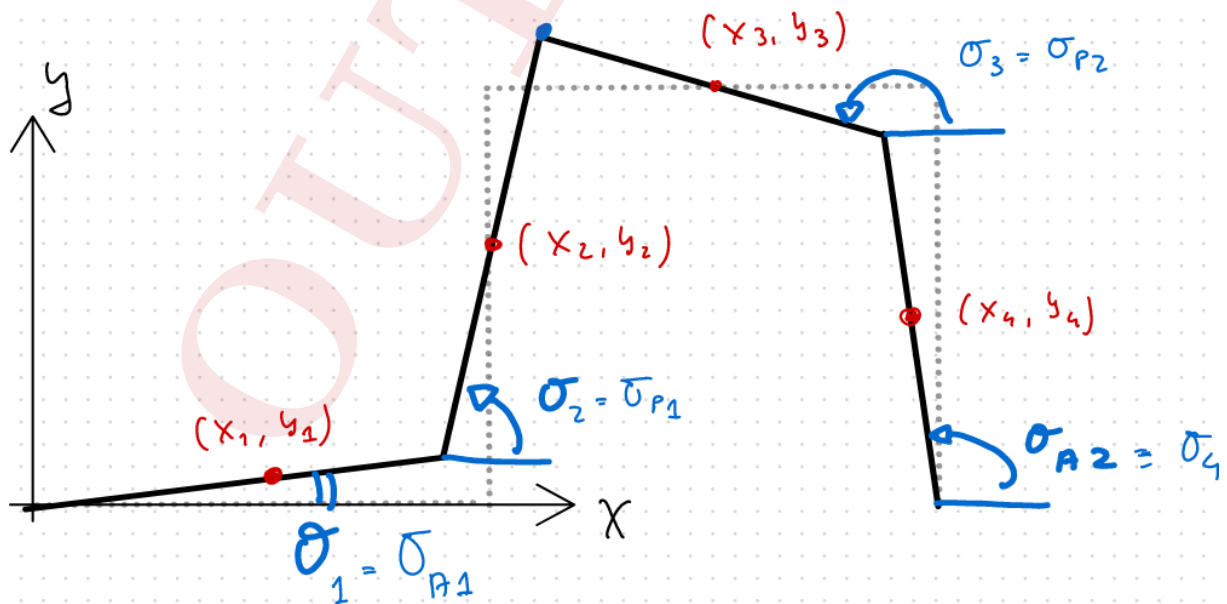
Where  $[m_{ph}] = [m, m, J_l + r^2 J_r, m, m, J_l, m, m, J_l, m, m, J_l + r^2 J_r]^T$

(n.b:  $J_l$  is the moment of inertia of the links at the center of gravity, do not use the Huygens–Steiner theorem or that other moment of inertia around the pivot)

(n.n.b:  $J_r$  is the moment of inertia of rotor moved on the load shaft)

and  $\dot{\underline{y}} = [x_{11}, y_{11}, \theta_{11}, x_{12}, y_{12}, \theta_{12}, x_{13}, y_{13}, \theta_{13}, x_{14}, y_{14}, \theta_{14}]^T$

is the vector of independent coordinates of the bodies according to this diagram:



We can describe  $\dot{\underline{y}}$  in terms of our 2 dof  $[q_1, q_2]^T = [\theta_{A1}, \theta_{A2}]^T$  via a Jacobian matrix  $[\Lambda_m]$ :

$$\underline{\dot{y}} = [\Lambda_m] \underline{\dot{q}} \quad 2.$$

The new system will be:

$$T = \frac{1}{2} \underline{\dot{y}}^T [m_{ph}] \underline{\dot{y}} = \frac{1}{2} \underline{\dot{q}}^T [m_0] \underline{\dot{q}} \quad 3.$$

With  $[m_0] = [\Lambda_m]^T [m_{ph}] [\Lambda_m]$

The kinetic term of the Lagrangian equation becomes:

$$\frac{d}{dt} \left( \frac{\partial T}{\partial \underline{\dot{q}}} \right)^T - \left( \frac{\partial T}{\partial \underline{q}} \right)^T = [m_0] \underline{\ddot{q}} \quad 4.$$

We can then calculate the work of the time dependent forces (our servo actuators):

$$\delta W = \delta \underline{y}_f^T \underline{f}_{ph} = [\delta \theta_{A1}, \delta \theta_{A2}] \begin{bmatrix} \tau_1 \\ \tau_2 \end{bmatrix} = [\delta q_1, \delta q_2] \begin{bmatrix} \tau_1 \\ \tau_2 \end{bmatrix} = \delta \underline{q}^T \underline{f}_{ph} \quad 5.$$

(In this case  $[\Lambda_f]$  is simply the identity matrix)

$$\underline{f}(t) = [\Lambda_f]^T \underline{f}_{ph} = \underline{f}_{ph} \quad 6.$$

Our Lagrange equation becomes:

$$[m_0] \underline{\ddot{q}} = \underline{f}(t) \quad 7.$$

$$\begin{bmatrix} \tau_1 \\ \tau_2 \end{bmatrix} = \begin{bmatrix} m_{11} & m_{12} \\ m_{21} & m_{22} \end{bmatrix} \begin{bmatrix} \ddot{q}_1 \\ \ddot{q}_2 \end{bmatrix} \quad 8.$$

With these equations we can calculate the torque applied on the load shafts when a specific angular acceleration occurs (or if we invert it, the necessary torque to have a desired acceleration on the load shafts).

This is a good starting point to analyze eventual cross interactions between the two shafts.

### 3.1) The humble Jacobian of Inertia

The system has 4 links (4x3 DOF = 12 DOF) and 5 revolute joints (each constraining 2 DOF => -10 DOF) : in total we have 2 DOF

Our Jacobian will be a 12x2 matrix

$$[\Lambda_m] = \begin{bmatrix} \lambda_{1,1} & \lambda_{1,2} \\ \lambda_{2,1} & \lambda_{2,2} \\ \lambda_{3,1} & \lambda_{3,2} \\ \lambda_{4,1} & \lambda_{4,2} \\ \lambda_{5,1} & \lambda_{5,2} \\ \lambda_{6,1} & \lambda_{6,2} \\ \lambda_{7,1} & \lambda_{7,2} \\ \lambda_{8,1} & \lambda_{8,2} \\ \lambda_{9,1} & \lambda_{9,2} \\ \lambda_{10,1} & \lambda_{10,2} \\ \lambda_{11,1} & \lambda_{11,2} \\ \lambda_{12,1} & \lambda_{12,2} \end{bmatrix} = \begin{bmatrix} -\frac{L}{2} \sin(\theta_{A1}) & 0 \\ +\frac{L}{2} \cos(\theta_{A1}) & 0 \\ 1 & 0 \\ \lambda_{4,1} & \lambda_{4,2} \\ \lambda_{5,1} & \lambda_{5,2} \\ \lambda_{6,1} & \lambda_{6,2} \\ \lambda_{7,1} & \lambda_{7,2} \\ \lambda_{8,1} & \lambda_{8,2} \\ \lambda_{9,1} & \lambda_{9,2} \\ 0 & -\frac{L}{2} \sin(\theta_{A2}) \\ 0 & +\frac{L}{2} \cos(\theta_{A2}) \\ 0 & 1 \end{bmatrix}$$

The remaining terms needs to be calculated keeping in mind the inverse kinematics, which is cumbersome by hand. I used the MATLAB Symbolic Math Toolbox. For this reason they are *slightly longer* and are left in the appendix for clarity.

With our Jacobian we can then calculate the generalized mass  $[m_0]$  (again with the Symbolic Toolbox)

#### 4) How decoupled are we?

$$\begin{bmatrix} \tau_1 \\ \tau_2 \end{bmatrix} = \begin{bmatrix} m_{11} & m_{12} \\ m_{21} & m_{22} \end{bmatrix} \begin{bmatrix} \ddot{q}_1 \\ \ddot{q}_2 \end{bmatrix} \quad 9.$$

Let's bring back the Lagrange equation and see what happens at the "resting position":

```
rgaf(0,pi/2,true)
```

$$[m_0](\text{rest}) = \begin{bmatrix} 10.2287 & 0.0002 \\ 0.0002 & 10.2271 \end{bmatrix} \quad 10.$$

So, to obtain  $1 \frac{\text{rad}}{\text{s}^2}$  of acceleration on the 1st active link we need 10.2287 Nm on the 1st load shaft and 0.0002 Nm on the 2nd load shaft (which when accounting for the  $r = 70$  gear ratio results in  $0.1461 \text{ Nm}$  and  $2.8571 \times 10^{-6}$  on the motor shafts respectively)

Dually, by inverting we have:

$$\begin{bmatrix} \ddot{q}_1 \\ \ddot{q}_2 \end{bmatrix} = [m_0]^{-1} \begin{bmatrix} \tau_1 \\ \tau_2 \end{bmatrix} \quad 11.$$

$$[m_0]^{-1}(\text{rest}) = \begin{bmatrix} 0.0978 & -0.0000 \\ -0.0000 & 0.0978 \end{bmatrix} \quad 12.$$

Which means that when applying  $1 \text{ Nm}$  on the 1st active load shaft we'll end up with  $0.0978 \frac{\text{rad}}{\text{s}^2}$  on the first active link and a negligible acceleration on the second load shaft. **Great!**

Be aware that symbolically inverting  $[m_0]$  is useless because we can just invert the matrix after the evaluation.

#### 5) Relative gain array analysis

##### Relative gain array

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The **relative gain array** (RGA) is a classical widely-used<sup>[*citation needed*]</sup> method for determining the best input-output pairings for multivariable **process control** systems.<sup>[1]</sup> It has many practical open-loop and closed-loop control applications and is relevant to analyzing many fundamental steady-state closed-loop system properties such as stability and robustness.<sup>[2]</sup>

Standard control theory method to evaluate the decoupling (or not) of a MIMO system. I only have these slides in Italian, I'm sorry guys :(

## - MATRICE DEI GUADAGNI RELATIVI (RGA, RELATIVE GAIN ARRAY)

- UTILE PER:
  - VALUTARE IL GRADO DI INTERAZIONE
  - SCEGLIERE I MIGLIORI ACCOPPIAMENTI I/O

### - IPOTESI

1.  $G(s)$  A.S. STABILE
2.  $\det G(0) \neq 0$

### - DEFINIZIONE

(RGA)

$$\Lambda = G(0) \odot (G(0)^{-1})'$$

MATRICE  $m \times m$

PRODOTTO DI SCHUR  
(ELEMENTO PER ELEMENTO)

( $\odot$  HADAMARD)

- SE  $\Lambda \approx I_m \Rightarrow$  INTERAZIONE DEBOLE  
CON GLI ACCOPPIAMENTI  $\{u_i, y_i\}$

### - CASO $m=2$

$$G(0) = \begin{bmatrix} \mu_{11} & \mu_{12} \\ \mu_{21} & \mu_{22} \end{bmatrix}$$

$$G(0)^{-1} = \frac{1}{\det G(0)} \begin{bmatrix} \mu_{22} & -\mu_{12} \\ -\mu_{21} & \mu_{11} \end{bmatrix}$$

$$(G(0)^{-1})' = \frac{1}{\det G(0)} \begin{bmatrix} \mu_{22} & -\mu_{21} \\ -\mu_{12} & \mu_{11} \end{bmatrix} \quad \det G(0) = \mu_{11}\mu_{22} - \mu_{12}\mu_{21}$$

$$\Lambda = G(0) \odot (G(0)^{-1})' = \frac{1}{\det G(0)} \begin{bmatrix} \mu_{11}\mu_{22} & -\mu_{12}\mu_{21} \\ -\mu_{12}\mu_{21} & \mu_{11}\mu_{22} \end{bmatrix}$$

- PONEENDO  $\lambda = \frac{\mu_{11}\mu_{22}}{\det G(0)} \Rightarrow \Lambda = \begin{bmatrix} \lambda & 1-\lambda \\ 1-\lambda & \lambda \end{bmatrix}$

- SE  $\lambda = 1 \Rightarrow \Lambda = I_2$  ✓

$\lambda = 0 \Rightarrow \Lambda = \begin{bmatrix} 0 & 1 \\ 1 & 0 \end{bmatrix}$

MA, SCAMBIANDO GLI INGRESSI  $u_i \Rightarrow \bar{\Lambda} = I_2$

- CASO  $m=2$  (SEGUE)

$$\mathcal{L} = \begin{bmatrix} \lambda & 1-\lambda \\ 1-\lambda & \lambda \end{bmatrix}$$

$$\bar{\mathcal{L}} = \begin{bmatrix} 1-\lambda & \lambda \\ \lambda & 1-\lambda \end{bmatrix}$$

(A) COPPIE  $\{u_1, y_1\}, \{u_2, y_2\}$

(B) COPPIE  $\{u_1, y_2\}, \{u_2, y_1\}$

- REGOLA DI SCELTA

$$\lambda = 1 \Rightarrow \text{(A)}$$

$$\lambda = 0 \Rightarrow \text{(B)}$$

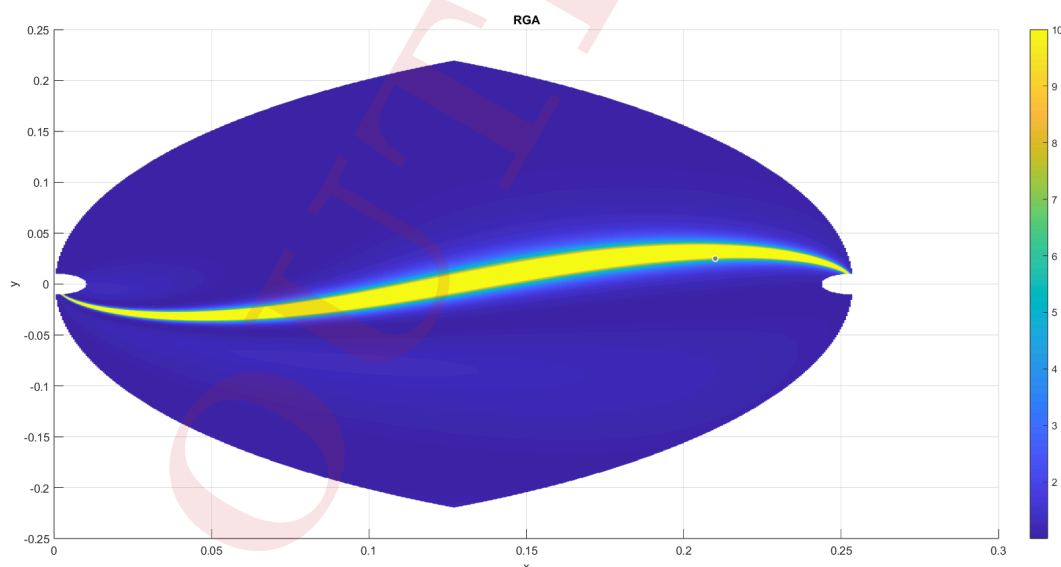
$$\lambda > \frac{1}{2} \Rightarrow \text{MEGLIO (A) CHE (B)}$$

$$\lambda < \frac{1}{2} \Rightarrow \text{MEGLIO (B) CHE (A)}$$

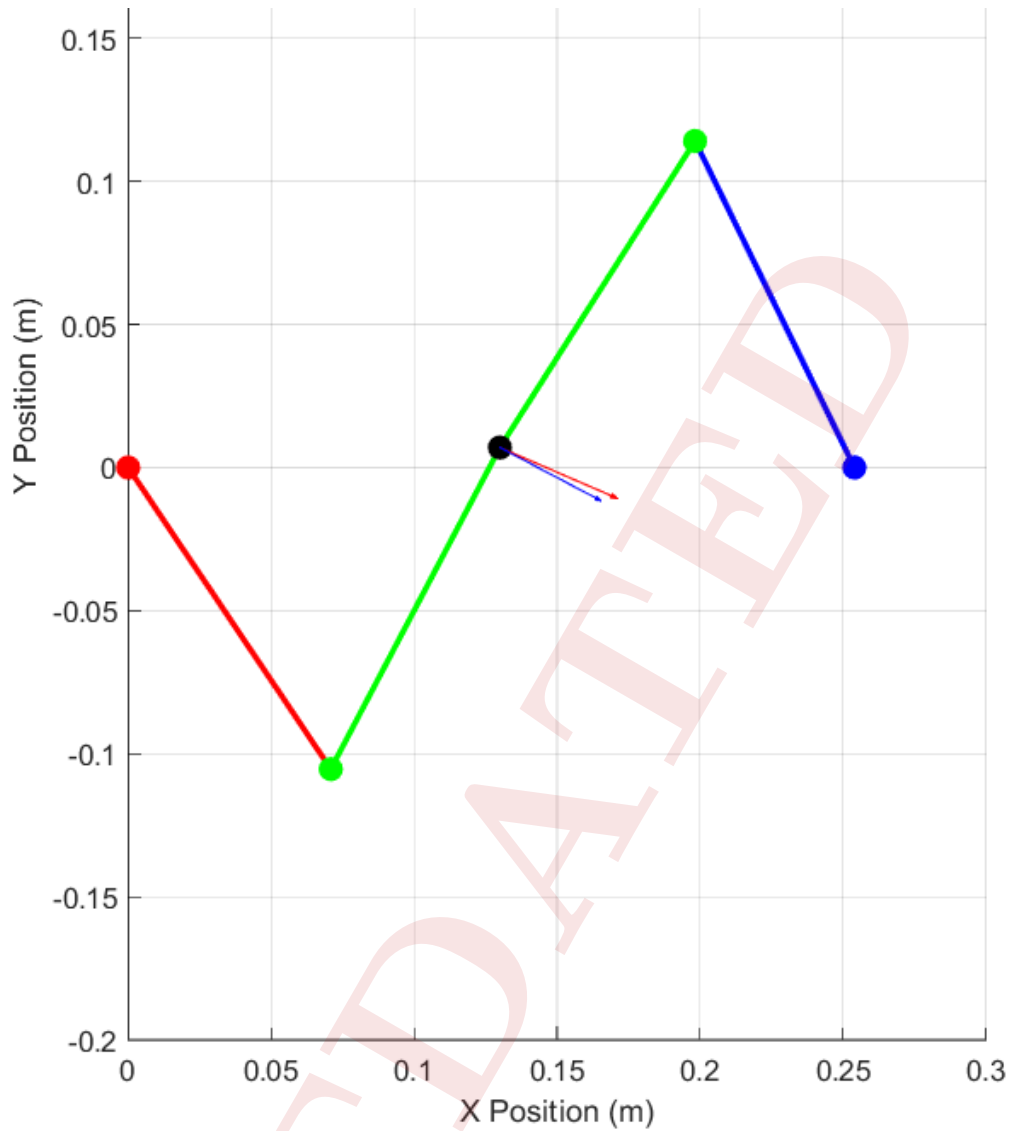
$$\left. \begin{array}{l} \lambda \gg 1 \\ \lambda \ll 0 \end{array} \right\} \Rightarrow \text{FORTE INTERAZIONE}$$

## 5.1) Analysis Approach

Let's plot  $\lambda_{\text{rga}}$  on the Cartesian workspace. When  $\lambda_{\text{rga}} \approx 1$  it means we have high decoupling, otherwise we have cross-coupling between the active links:



We can see how we have good decoupling everywhere but in the singularity region, which is great and makes sense if you think about it:



When near the singularity, every torque applied on one shaft is fully transferred to the other shaft = high RGA!

## 6) Appendix

### 6.1) Jacobian terms

```
jac(4,1) = - L*sin(ta1) + (sin(angle(L*(sin(ta1) - sin(ta2))*(- 1 - li)) +
acos((L^2*(cos(ta2) - cos(ta1) + 2)^2 + L^2*(sin(ta1) - sin(ta2))^2)^(1/2)/
(2*L)))*(2*L^2*sin(ta1)*(cos(ta2) - cos(ta1) + 2) + 2*L^2*cos(ta1)*(sin(ta1) -
sin(ta2))))/(8*(L^2*(cos(ta2) - cos(ta1) + 2)^2 + L^2*(sin(ta1) -
sin(ta2))^2)^(1/2)*(1 - (L^2*(cos(ta2) - cos(ta1) + 2)^2 + L^2*(sin(ta1) -
sin(ta2))^2)/(4*L^2))^(1/2));
```

```
jac(5,1) = L*cos(ta1) - (cos(angle(L*(sin(ta1) - sin(ta2))*(- 1 - li)) +
acos((L^2*(cos(ta2) - cos(ta1) + 2)^2 + L^2*(sin(ta1) - sin(ta2))^2)^(1/2)/
(2*L)))*(2*L^2*sin(ta1)*(cos(ta2) - cos(ta1) + 2) + 2*L^2*cos(ta1)*(sin(ta1) -
sin(ta2))))/(8*(L^2*(cos(ta2) - cos(ta1) + 2)^2 + L^2*(sin(ta1) -
sin(ta2))^2)^(1/2)*(1 - (L^2*(cos(ta2) - cos(ta1) + 2)^2 + L^2*(sin(ta1) -
sin(ta2))^2)/(4*L^2))^(1/2));
```

```
jac(6,1) = -(2*L^2*sin(ta1)*(cos(ta2) - cos(ta1) + 2) + 2*L^2*cos(ta1)*(sin(ta1) -
sin(ta2)))/(4*L*(L^2*(cos(ta2) - cos(ta1) + 2)^2 + L^2*(sin(ta1) -
sin(ta2))^2)^(1/2)*(1 - (L^2*(cos(ta2) - cos(ta1) + 2)^2 + L^2*(sin(ta1) -
sin(ta2))^2)/(4*L^2))^(1/2));
```

```
jac(7,1) = -L*sin(ta1) + (sin(angle(L*(sin(ta1) - sin(ta2)))*(-1 - li)) +
acos((L^2*(cos(ta2) - cos(ta1) + 2)^2 + L^2*(sin(ta1) - sin(ta2))^2)^(1/2)/
(2*L)))*(2*L^2*sin(ta1)*(cos(ta2) - cos(ta1) + 2) + 2*L^2*cos(ta1)*(sin(ta1) -
sin(ta2)))/(4*(L^2*(cos(ta2) - cos(ta1) + 2)^2 + L^2*(sin(ta1) -
sin(ta2))^2)^(1/2)*(1 - (L^2*(cos(ta2) - cos(ta1) + 2)^2 + L^2*(sin(ta1) -
sin(ta2))^2)/(4*L^2))^(1/2)) - (sin(angle(L*(sin(ta1) - sin(ta2)))*(-1 - li)) -
acos((L^2*(cos(ta2) - cos(ta1) + 2)^2 + L^2*(sin(ta1) - sin(ta2))^2)^(1/2)/
(2*L)))*(2*L^2*sin(ta1)*(cos(ta2) - cos(ta1) + 2) + 2*L^2*cos(ta1)*(sin(ta1) -
sin(ta2)))/(8*(L^2*(cos(ta2) - cos(ta1) + 2)^2 + L^2*(sin(ta1) -
sin(ta2))^2)^(1/2)*(1 - (L^2*(cos(ta2) - cos(ta1) + 2)^2 + L^2*(sin(ta1) -
sin(ta2))^2)/(4*L^2))^(1/2));
```

```
jac(8,1) = L*cos(ta1) - (cos(angle(L*(sin(ta1) - sin(ta2)))*(-1 - li)) +
acos((L^2*(cos(ta2) - cos(ta1) + 2)^2 + L^2*(sin(ta1) - sin(ta2))^2)^(1/2)/
(2*L)))*(2*L^2*sin(ta1)*(cos(ta2) - cos(ta1) + 2) + 2*L^2*cos(ta1)*(sin(ta1) -
sin(ta2)))/(4*(L^2*(cos(ta2) - cos(ta1) + 2)^2 + L^2*(sin(ta1) -
sin(ta2))^2)^(1/2)*(1 - (L^2*(cos(ta2) - cos(ta1) + 2)^2 + L^2*(sin(ta1) -
sin(ta2))^2)/(4*L^2))^(1/2)) + (cos(angle(L*(sin(ta1) - sin(ta2)))*(-1 - li)) -
acos((L^2*(cos(ta2) - cos(ta1) + 2)^2 + L^2*(sin(ta1) - sin(ta2))^2)^(1/2)/
(2*L)))*(2*L^2*sin(ta1)*(cos(ta2) - cos(ta1) + 2) + 2*L^2*cos(ta1)*(sin(ta1) -
sin(ta2)))/(8*(L^2*(cos(ta2) - cos(ta1) + 2)^2 + L^2*(sin(ta1) -
sin(ta2))^2)^(1/2)*(1 - (L^2*(cos(ta2) - cos(ta1) + 2)^2 + L^2*(sin(ta1) -
sin(ta2))^2)/(4*L^2))^(1/2));
```

```
jac(9,1) = (2*L^2*sin(ta1)*(cos(ta2) - cos(ta1) + 2) + 2*L^2*cos(ta1)*(sin(ta1) -
sin(ta2)))/(4*L*(L^2*(cos(ta2) - cos(ta1) + 2)^2 + L^2*(sin(ta1) -
sin(ta2))^2)^(1/2)*(1 - (L^2*(cos(ta2) - cos(ta1) + 2)^2 + L^2*(sin(ta1) -
sin(ta2))^2)/(4*L^2))^(1/2));
```

```
jac(4,2) = -(sin(angle(L*(sin(ta1) - sin(ta2)))*(-1 - li)) + acos((L^2*(cos(ta2) -
cos(ta1) + 2)^2 + L^2*(sin(ta1) - sin(ta2))^2)^(1/2)/
(2*L)))*(2*L^2*sin(ta2)*(cos(ta2) - cos(ta1) + 2) + 2*L^2*cos(ta2)*(sin(ta1) -
sin(ta2)))/(8*(L^2*(cos(ta2) - cos(ta1) + 2)^2 + L^2*(sin(ta1) -
sin(ta2))^2)^(1/2)*(1 - (L^2*(cos(ta2) - cos(ta1) + 2)^2 + L^2*(sin(ta1) -
sin(ta2))^2)/(4*L^2))^(1/2));
```

```
jac(5,2) = (cos(angle(L*(sin(ta1) - sin(ta2)))*(-1 - li)) + acos((L^2*(cos(ta2) -
cos(ta1) + 2)^2 + L^2*(sin(ta1) - sin(ta2))^2)^(1/2)/
(2*L)))*(2*L^2*sin(ta2)*(cos(ta2) - cos(ta1) + 2) + 2*L^2*cos(ta2)*(sin(ta1) -
sin(ta2)))/(8*(L^2*(cos(ta2) - cos(ta1) + 2)^2 + L^2*(sin(ta1) -
sin(ta2))^2)^(1/2)*(1 - (L^2*(cos(ta2) - cos(ta1) + 2)^2 + L^2*(sin(ta1) -
sin(ta2))^2)/(4*L^2))^(1/2));
```

```
jac(6,2) = (2*L^2*sin(ta2)*(cos(ta2) - cos(ta1) + 2) + 2*L^2*cos(ta2)*(sin(ta1) -
sin(ta2)))/(4*L*(L^2*(cos(ta2) - cos(ta1) + 2)^2 + L^2*(sin(ta1) -
sin(ta2))^2)^(1/2)*(1 - (L^2*(cos(ta2) - cos(ta1) + 2)^2 + L^2*(sin(ta1) -
sin(ta2))^2)/(4*L^2))^(1/2));
```

```
jac(7,2) = - (sin(angle(L*(sin(ta1) - sin(ta2)))*(-1 - li)) + acos((L^2*(cos(ta2) -
cos(ta1) + 2)^2 + L^2*(sin(ta1) - sin(ta2))^2)^(1/2)/
(2*L)))*(2*L^2*sin(ta2)*(cos(ta2) - cos(ta1) + 2) + 2*L^2*cos(ta2)*(sin(ta1) -
sin(ta2)))/(4*(L^2*(cos(ta2) - cos(ta1) + 2)^2 + L^2*(sin(ta1) -
```

```
sin(ta2))^2)^(1/2)*(1 - (L^2*(cos(ta2) - cos(ta1) + 2)^2 + L^2*(sin(ta1) -
sin(ta2))^2)/(4*L^2))^(1/2)) + (sin(angle(L*(sin(ta1) - sin(ta2))*(- 1 - li)) -
acos((L^2*(cos(ta2) - cos(ta1) + 2)^2 + L^2*(sin(ta1) - sin(ta2))^2)^(1/2)/
(2*L)))*(2*L^2*sin(ta2)*(cos(ta2) - cos(ta1) + 2) + 2*L^2*cos(ta2)*(sin(ta1) -
sin(ta2))))/(8*(L^2*(cos(ta2) - cos(ta1) + 2)^2 + L^2*(sin(ta1) -
sin(ta2))^2)^(1/2)*(1 - (L^2*(cos(ta2) - cos(ta1) + 2)^2 + L^2*(sin(ta1) -
sin(ta2))^2)/(4*L^2))^(1/2));
```

```
jac(8,2) = (cos(angle(L*(sin(ta1) - sin(ta2))*(- 1 - li)) + acos((L^2*(cos(ta2) - cos(ta1) + 2)^2 + L^2*(sin(ta1) - sin(ta2))^2)^(1/2)/(2*L)))*(2*L^2*sin(ta2)*(cos(ta2) - cos(ta1) + 2) + 2*L^2*cos(ta2)*(sin(ta1) - sin(ta2))))/(4*(L^2*(cos(ta2) - cos(ta1) + 2)^2 + L^2*(sin(ta1) - sin(ta2))^2)^(1/2)*(1 - (L^2*(cos(ta2) - cos(ta1) + 2)^2 + L^2*(sin(ta1) - sin(ta2))^2)/(4*L^2))^(1/2)) - (cos(angle(L*(sin(ta1) - sin(ta2))*(- 1 - li)) + acos((L^2*(cos(ta2) - cos(ta1) + 2)^2 + L^2*(sin(ta1) - sin(ta2))^2)^(1/2)/(2*L)))*(2*L^2*sin(ta2)*(cos(ta2) - cos(ta1) + 2) + 2*L^2*cos(ta2)*(sin(ta1) - sin(ta2))))/(8*(L^2*(cos(ta2) - cos(ta1) + 2)^2 + L^2*(sin(ta1) - sin(ta2))^2)^(1/2)*(1 - (L^2*(cos(ta2) - cos(ta1) + 2)^2 + L^2*(sin(ta1) - sin(ta2))^2)/(4*L^2))^(1/2));
```

```
jac(9,2) = -(2*L^2*sin(ta2)*(cos(ta2) - cos(ta1) + 2) + 2*L^2*cos(ta2)*(sin(ta1) - sin(ta2)))/(4*L*(L^2*(cos(ta2) - cos(ta1) + 2)^2 + L^2*(sin(ta1) - sin(ta2))^2)^(1/2)*(1 - (L^2*(cos(ta2) - cos(ta1) + 2)^2 + L^2*(sin(ta1) - sin(ta2))^2)/(4*L^2))^(1/2));
```

## 6.2) Generalized Mass

```
mm(1,1) = Ja + M*(L*cos(ta1) - (cos(angle(L*(sin(ta1) - sin(ta2))*(- 1 - li)) +
acos((L^2*(cos(ta2) - cos(ta1) + 2)^2 + L^2*(sin(ta1) - sin(ta2))^2)^(1/2)/
(2*L)))*(2*L^2*sin(ta1)*(cos(ta2) - cos(ta1) + 2) + 2*L^2*cos(ta1)*(sin(ta1) -
sin(ta2))))/(4*(L^2*(cos(ta2) - cos(ta1) + 2)^2 + L^2*(sin(ta1) -
sin(ta2))^2)^(1/2)*(1 - (L^2*(cos(ta2) - cos(ta1) + 2)^2 + L^2*(sin(ta1) -
sin(ta2))^2)/(4*L^2))^(1/2)) + (cos(angle(L*(sin(ta1) - sin(ta2))*(- 1 - li)) -
acos((L^2*(cos(ta2) - cos(ta1) + 2)^2 + L^2*(sin(ta1) - sin(ta2))^2)^(1/2)/
(2*L)))*(2*L^2*sin(ta1)*(cos(ta2) - cos(ta1) + 2) + 2*L^2*cos(ta1)*(sin(ta1) -
sin(ta2))))/(8*(L^2*(cos(ta2) - cos(ta1) + 2)^2 + L^2*(sin(ta1) -
sin(ta2))^2)^(1/2)*(1 - (L^2*(cos(ta2) - cos(ta1) + 2)^2 + L^2*(sin(ta1) -
sin(ta2))^2)/(4*L^2))^(1/2)))*(L*cos(ta1) - (cos(conj(acos((L^2*(cos(ta2) - cos(ta1)
+ 2)^2 + L^2*(sin(ta1) - sin(ta2))^2)^(1/2)/(2*L))) + angle(L*(sin(ta1) -
sin(ta2))*(- 1 - li)))*(2*L^2*sin(ta1)*(cos(ta2) - cos(ta1) + 2) +
2*L^2*cos(ta1)*(sin(ta1) - sin(ta2))))/(4*conj((1 - (L^2*(cos(ta2) - cos(ta1) + 2)^2
+ L^2*(sin(ta1) - sin(ta2))^2)/(4*L^2))^(1/2))*(L^2*(cos(ta2) - cos(ta1) + 2)^2 +
L^2*(sin(ta1) - sin(ta2))^2)^(1/2)) + (cos(conj(acos((L^2*(cos(ta2) - cos(ta1) + 2)^2
+ L^2*(sin(ta1) - sin(ta2))^2)^(1/2)/(2*L))) - angle(L*(sin(ta1) - sin(ta2))*(- 1 -
li)))*(2*L^2*sin(ta1)*(cos(ta2) - cos(ta1) + 2) + 2*L^2*cos(ta1)*(sin(ta1) -
sin(ta2))))/(8*conj((1 - (L^2*(cos(ta2) - cos(ta1) + 2)^2 + L^2*(sin(ta1) -
sin(ta2))^2)/(4*L^2))^(1/2))*(L^2*(cos(ta2) - cos(ta1) + 2)^2 + L^2*(sin(ta1) -
sin(ta2))^2)^(1/2))) + M*(L*cos(ta1) - (cos(angle(L*(sin(ta1) - sin(ta2))*(- 1 - li))
+ acos((L^2*(cos(ta2) - cos(ta1) + 2)^2 + L^2*(sin(ta1) - sin(ta2))^2)^(1/2)/
(2*L)))*(2*L^2*sin(ta1)*(cos(ta2) - cos(ta1) + 2) + 2*L^2*cos(ta1)*(sin(ta1) -
sin(ta2))))/(8*(L^2*(cos(ta2) - cos(ta1) + 2)^2 + L^2*(sin(ta1) -
sin(ta2))^2)^(1/2)*(1 - (L^2*(cos(ta2) - cos(ta1) + 2)^2 + L^2*(sin(ta1) -
sin(ta2))^2)/(4*L^2))^(1/2)))*(L*cos(ta1) - (cos(conj(acos((L^2*(cos(ta2) - cos(ta1)
+ 2)^2 + L^2*(sin(ta1) - sin(ta2))^2)^(1/2)/(2*L))) + angle(L*(sin(ta1) -
sin(ta2))*(- 1 - li)))*(2*L^2*sin(ta1)*(cos(ta2) - cos(ta1) + 2) +
2*L^2*cos(ta1)*(sin(ta1) - sin(ta2))))/(8*conj((1 - (L^2*(cos(ta2) - cos(ta1) + 2)^2
+ L^2*(sin(ta1) - sin(ta2))^2)/(4*L^2))^(1/2))*(L^2*(cos(ta2) - cos(ta1) + 2)^2 +
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L^2*(sin(ta1) - sin(ta2))^2*(1/2))) + (L^2*M*cos(ta1)^2)/4 + (L^2*M*sin(ta1)^2)/4 -
M*(L*sin(ta1) - (sin(angle(L*(sin(ta1) - sin(ta2))*(- 1 - li)) + acos((L^2*(cos(ta2)
- cos(ta1) + 2)^2 + L^2*(sin(ta1) - sin(ta2))^2)^(1/2)/
(2*L)))*(2*L^2*sin(ta1)*(cos(ta2) - cos(ta1) + 2) + 2*L^2*cos(ta1)*(sin(ta1) -
sin(ta2))))/(4*(L^2*(cos(ta2) - cos(ta1) + 2)^2 + L^2*(sin(ta1) -
sin(ta2))^2)^(1/2)*(1 - (L^2*(cos(ta2) - cos(ta1) + 2)^2 + L^2*(sin(ta1) -
sin(ta2))^2)/(4*L^2))^(1/2))) + (sin(angle(L*(sin(ta1) - sin(ta2))*(- 1 - li)) -
acos((L^2*(cos(ta2) - cos(ta1) + 2)^2 + L^2*(sin(ta1) - sin(ta2))^2)^(1/2)/
(2*L)))*(2*L^2*sin(ta1)*(cos(ta2) - cos(ta1) + 2) + 2*L^2*cos(ta1)*(sin(ta1) -
sin(ta2))))/(8*(L^2*(cos(ta2) - cos(ta1) + 2)^2 + L^2*(sin(ta1) -
sin(ta2))^2)^(1/2)*(1 - (L^2*(cos(ta2) - cos(ta1) + 2)^2 + L^2*(sin(ta1) -
sin(ta2))^2)/(4*L^2))^(1/2)))*(- L*sin(ta1) + (sin(conj(acos((L^2*(cos(ta2) -
cos(ta1) + 2)^2 + L^2*(sin(ta1) - sin(ta2))^2)^(1/2)/(2*L))) - angle(L*(sin(ta1) -
sin(ta2))*(- 1 - li)))*(2*L^2*sin(ta1)*(cos(ta2) - cos(ta1) + 2) +
2*L^2*cos(ta1)*(sin(ta1) - sin(ta2))))/(8*conj((1 - (L^2*(cos(ta2) - cos(ta1) + 2)^2
+ L^2*(sin(ta1) - sin(ta2))^2)/(4*L^2))^(1/2))*(L^2*(cos(ta2) - cos(ta1) + 2)^2 +
L^2*(sin(ta1) - sin(ta2))^2)^(1/2))) + (sin(conj(acos((L^2*(cos(ta2) - cos(ta1) + 2)^2
+ L^2*(sin(ta1) - sin(ta2))^2)^(1/2)/(2*L))) + angle(L*(sin(ta1) - sin(ta2))*(- 1 -
li)))*(2*L^2*sin(ta1)*(cos(ta2) - cos(ta1) + 2) + 2*L^2*cos(ta1)*(sin(ta1) -
sin(ta2))))/(4*conj((1 - (L^2*(cos(ta2) - cos(ta1) + 2)^2 + L^2*(sin(ta1) -
sin(ta2))^2)/(4*L^2))^(1/2))*(L^2*(cos(ta2) - cos(ta1) + 2)^2 + L^2*(sin(ta1) -
sin(ta2))^2)^(1/2))) + M*(L*sin(ta1) - (sin(angle(L*(sin(ta1) - sin(ta2))*(- 1 - li))
+ acos((L^2*(cos(ta2) - cos(ta1) + 2)^2 + L^2*(sin(ta1) - sin(ta2))^2)^(1/2)/
(2*L)))*(2*L^2*sin(ta1)*(cos(ta2) - cos(ta1) + 2) + 2*L^2*cos(ta1)*(sin(ta1) -
sin(ta2))))/(8*(L^2*(cos(ta2) - cos(ta1) + 2)^2 + L^2*(sin(ta1) -
sin(ta2))^2)^(1/2)*(1 - (L^2*(cos(ta2) - cos(ta1) + 2)^2 + L^2*(sin(ta1) -
sin(ta2))^2)/(4*L^2))^(1/2)))*(L*sin(ta1) - (sin(conj(acos((L^2*(cos(ta2) - cos(ta1)
+ 2)^2 + L^2*(sin(ta1) - sin(ta2))^2)^(1/2)/(2*L))) + angle(L*(sin(ta1) -
sin(ta2))*(- 1 - li)))*(2*L^2*sin(ta1)*(cos(ta2) - cos(ta1) + 2) +
2*L^2*cos(ta1)*(sin(ta1) - sin(ta2))))/(8*conj((1 - (L^2*(cos(ta2) - cos(ta1) + 2)^2
+ L^2*(sin(ta1) - sin(ta2))^2)/(4*L^2))^(1/2))*(L^2*(cos(ta2) - cos(ta1) + 2)^2 +
L^2*(sin(ta1) - sin(ta2))^2)^(1/2))) + (Jp*(2*L^2*sin(ta1)*(cos(ta2) - cos(ta1) + 2)
+ 2*L^2*cos(ta1)*(sin(ta1) - sin(ta2)))^2)/(8*L^2*conj((1 - (L^2*(cos(ta2) - cos(ta1)
+ 2)^2 + L^2*(sin(ta1) - sin(ta2))^2)/(4*L^2))^(1/2))*(L^2*(cos(ta2) - cos(ta1) +
2)^2 + L^2*(sin(ta1) - sin(ta2))^2)*(1 - (L^2*(cos(ta2) - cos(ta1) + 2)^2 +
L^2*(sin(ta1) - sin(ta2))^2)/(4*L^2))^(1/2));

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$$\begin{aligned} \text{mm}(1,2) = & -M * ((\sin(\text{angle}(L * (\sin(\text{ta1}) - \sin(\text{ta2})) * (-1 - 1i))) + \text{acos}((L^2 * (\cos(\text{ta2}) \\ & - \cos(\text{ta1}) + 2)^2 + L^2 * (\sin(\text{ta1}) - \sin(\text{ta2}))^2)^{(1/2}) / \\ & (2 * L))) * (2 * L^2 * \sin(\text{ta2}) * (\cos(\text{ta2}) - \cos(\text{ta1}) + 2) + 2 * L^2 * \cos(\text{ta2}) * (\sin(\text{ta1}) - \\ & \sin(\text{ta2})))) / (4 * (L^2 * (\cos(\text{ta2}) - \cos(\text{ta1}) + 2)^2 + L^2 * (\sin(\text{ta1}) - \\ & \sin(\text{ta2}))^2)^{(1/2}) * (1 - (L^2 * (\cos(\text{ta2}) - \cos(\text{ta1}) + 2)^2 + L^2 * (\sin(\text{ta1}) - \\ & \sin(\text{ta2}))^2) / (4 * L^2))^{(1/2)}) - (\sin(\text{angle}(L * (\sin(\text{ta1}) - \sin(\text{ta2})) * (-1 - 1i))) - \\ & \text{acos}((L^2 * (\cos(\text{ta2}) - \cos(\text{ta1}) + 2)^2 + L^2 * (\sin(\text{ta1}) - \sin(\text{ta2}))^2)^{(1/2}) / \\ & (2 * L))) * (2 * L^2 * \sin(\text{ta2}) * (\cos(\text{ta2}) - \cos(\text{ta1}) + 2) + 2 * L^2 * \cos(\text{ta2}) * (\sin(\text{ta1}) - \\ & \sin(\text{ta2})))) / (8 * (L^2 * (\cos(\text{ta2}) - \cos(\text{ta1}) + 2)^2 + L^2 * (\sin(\text{ta1}) - \\ & \sin(\text{ta2}))^2)^{(1/2}) * (1 - (L^2 * (\cos(\text{ta2}) - \cos(\text{ta1}) + 2)^2 + L^2 * (\sin(\text{ta1}) - \\ & \sin(\text{ta2}))^2) / (4 * L^2))^{(1/2)})) * (-L * \sin(\text{ta1}) + (\sin(\text{conj}(\text{acos}((L^2 * (\cos(\text{ta2}) - \\ & \cos(\text{ta1}) + 2)^2 + L^2 * (\sin(\text{ta1}) - \sin(\text{ta2}))^2)^{(1/2}) / (2 * L))) - \text{angle}(L * (\sin(\text{ta1}) - \end{aligned}$$

[illegible]

[illegible]

$$\begin{aligned}
& (2*L))) * (2*L^2*\sin(ta1)*(\cos(ta2) - \cos(ta1) + 2) + 2*L^2*\cos(ta1)*(\sin(ta1) - \\
& \sin(ta2))) / (8*(L^2*(\cos(ta2) - \cos(ta1) + 2)^2 + L^2*(\sin(ta1) - \\
& \sin(ta2))^2)^{(1/2)} * (1 - (L^2*(\cos(ta2) - \cos(ta1) + 2)^2 + L^2*(\sin(ta1) - \\
& \sin(ta2))^2)/(4*L^2))^{(1/2)})) / (8*\text{conj}((1 - (L^2*(\cos(ta2) - \cos(ta1) + 2)^2 + \\
& L^2*(\sin(ta1) - \sin(ta2))^2)/(4*L^2))^{(1/2)}) * (L^2*(\cos(ta2) - \cos(ta1) + 2)^2 + \\
& L^2*(\sin(ta1) - \sin(ta2))^2)^{(1/2)}) - (\text{Jp}*(2*L^2*\sin(ta1)*(\cos(ta2) - \cos(ta1) + 2) + \\
& 2*L^2*\cos(ta1)*(\sin(ta1) - \sin(ta2))) * (2*L^2*\sin(ta2)*(\cos(ta2) - \cos(ta1) + 2) + \\
& 2*L^2*\cos(ta2)*(\sin(ta1) - \sin(ta2)))) / (8*L^2*\text{conj}((1 - (L^2*(\cos(ta2) - \cos(ta1) + \\
& 2)^2 + L^2*(\sin(ta1) - \sin(ta2))^2)/(4*L^2))^{(1/2)}) * (L^2*(\cos(ta2) - \cos(ta1) + 2)^2 + \\
& L^2*(\sin(ta1) - \sin(ta2))^2)^{(1/2)}) * (1 - (L^2*(\cos(ta2) - \cos(ta1) + 2)^2 + L^2*(\sin(ta1) \\
& - \sin(ta2))^2)/(4*L^2))^{(1/2)}) ;
\end{aligned}$$

$$\begin{aligned}
\text{mm}(2,2) = & \text{Ja} + \text{M}*((\cos(\text{angle}(L*(\sin(ta1) - \sin(ta2)))*(-1 - 1i)) + \\
& \text{acos}((L^2*(\cos(ta2) - \cos(ta1) + 2)^2 + L^2*(\sin(ta1) - \sin(ta2))^2)^{(1/2)} / \\
& (2*L))) * (2*L^2*\sin(ta2)*(\cos(ta2) - \cos(ta1) + 2) + 2*L^2*\cos(ta2)*(\sin(ta1) - \\
& \sin(ta2)))) / (4*(L^2*(\cos(ta2) - \cos(ta1) + 2)^2 + L^2*(\sin(ta1) - \\
& \sin(ta2))^2)^{(1/2)} * (1 - (L^2*(\cos(ta2) - \cos(ta1) + 2)^2 + L^2*(\sin(ta1) - \\
& \sin(ta2))^2)/(4*L^2))^{(1/2)}) - (\cos(\text{angle}(L*(\sin(ta1) - \sin(ta2)))*(-1 - 1i)) - \\
& \text{acos}((L^2*(\cos(ta2) - \cos(ta1) + 2)^2 + L^2*(\sin(ta1) - \sin(ta2))^2)^{(1/2)} / \\
& (2*L))) * (2*L^2*\sin(ta2)*(\cos(ta2) - \cos(ta1) + 2) + 2*L^2*\cos(ta2)*(\sin(ta1) - \\
& \sin(ta2)))) / (8*(L^2*(\cos(ta2) - \cos(ta1) + 2)^2 + L^2*(\sin(ta1) - \\
& \sin(ta2))^2)^{(1/2)} * (1 - (L^2*(\cos(ta2) - \cos(ta1) + 2)^2 + L^2*(\sin(ta1) - \\
& \sin(ta2))^2)/(4*L^2))^{(1/2)}) * ((\cos(\text{conj}(\text{acos}((L^2*(\cos(ta2) - \cos(ta1) + 2)^2 + \\
& L^2*(\sin(ta1) - \sin(ta2))^2)^{(1/2)} / (2*L))) + \text{angle}(L*(\sin(ta1) - \sin(ta2)))*(-1 - \\
& 1i))) * (2*L^2*\sin(ta2)*(\cos(ta2) - \cos(ta1) + 2) + 2*L^2*\cos(ta2)*(\sin(ta1) - \\
& \sin(ta2)))) / (4*\text{conj}((1 - (L^2*(\cos(ta2) - \cos(ta1) + 2)^2 + L^2*(\sin(ta1) - \\
& \sin(ta2))^2)/(4*L^2))^{(1/2)}) * (L^2*(\cos(ta2) - \cos(ta1) + 2)^2 + L^2*(\sin(ta1) - \\
& \sin(ta2))^2)^{(1/2)}) - (\cos(\text{conj}(\text{acos}((L^2*(\cos(ta2) - \cos(ta1) + 2)^2 + L^2*(\sin(ta1) \\
& - \sin(ta2))^2)^{(1/2)} / (2*L))) - \text{angle}(L*(\sin(ta1) - \sin(ta2)))*(-1 - \\
& 1i))) * (2*L^2*\sin(ta2)*(\cos(ta2) - \cos(ta1) + 2) + 2*L^2*\cos(ta2)*(\sin(ta1) - \\
& \sin(ta2)))) / (8*\text{conj}((1 - (L^2*(\cos(ta2) - \cos(ta1) + 2)^2 + L^2*(\sin(ta1) - \\
& \sin(ta2))^2)/(4*L^2))^{(1/2)}) * (L^2*(\cos(ta2) - \cos(ta1) + 2)^2 + L^2*(\sin(ta1) - \\
& \sin(ta2))^2)^{(1/2)})) + (L^2*\text{M}*\cos(ta2)^2)/4 + \text{M}*((\sin(\text{conj}(\text{acos}((L^2*(\cos(ta2) - \\
& \cos(ta1) + 2)^2 + L^2*(\sin(ta1) - \sin(ta2))^2)^{(1/2)} / (2*L))) - \text{angle}(L*(\sin(ta1) - \\
& \sin(ta2)))*(-1 - 1i))) * (2*L^2*\sin(ta2)*(\cos(ta2) - \cos(ta1) + 2) + \\
& 2*L^2*\cos(ta2)*(\sin(ta1) - \sin(ta2)))) / (8*\text{conj}((1 - (L^2*(\cos(ta2) - \cos(ta1) + 2)^2 + \\
& L^2*(\sin(ta1) - \sin(ta2))^2)/(4*L^2))^{(1/2)}) * (L^2*(\cos(ta2) - \cos(ta1) + 2)^2 + \\
& L^2*(\sin(ta1) - \sin(ta2))^2)^{(1/2)}) + (\sin(\text{conj}(\text{acos}((L^2*(\cos(ta2) - \cos(ta1) + 2)^2 + \\
& L^2*(\sin(ta1) - \sin(ta2))^2)^{(1/2)} / (2*L))) + \text{angle}(L*(\sin(ta1) - \sin(ta2)))*(-1 - \\
& 1i))) * (2*L^2*\sin(ta2)*(\cos(ta2) - \cos(ta1) + 2) + 2*L^2*\cos(ta2)*(\sin(ta1) - \\
& \sin(ta2)))) / (4*\text{conj}((1 - (L^2*(\cos(ta2) - \cos(ta1) + 2)^2 + L^2*(\sin(ta1) - \\
& \sin(ta2))^2)/(4*L^2))^{(1/2)}) * (L^2*(\cos(ta2) - \cos(ta1) + 2)^2 + L^2*(\sin(ta1) - \\
& \sin(ta2))^2)^{(1/2)})) * ((\sin(\text{angle}(L*(\sin(ta1) - \sin(ta2)))*(-1 - 1i)) + \\
& \text{acos}((L^2*(\cos(ta2) - \cos(ta1) + 2)^2 + L^2*(\sin(ta1) - \sin(ta2))^2)^{(1/2)} / \\
& (2*L))) * (2*L^2*\sin(ta2)*(\cos(ta2) - \cos(ta1) + 2) + 2*L^2*\cos(ta2)*(\sin(ta1) - \\
& \sin(ta2)))) / (4*(L^2*(\cos(ta2) - \cos(ta1) + 2)^2 + L^2*(\sin(ta1) - \\
& \sin(ta2))^2)^{(1/2)} * (1 - (L^2*(\cos(ta2) - \cos(ta1) + 2)^2 + L^2*(\sin(ta1) - \\
& \sin(ta2))^2)/(4*L^2))^{(1/2)}) - (\sin(\text{angle}(L*(\sin(ta1) - \sin(ta2)))*(-1 - 1i)) - \\
& \text{acos}((L^2*(\cos(ta2) - \cos(ta1) + 2)^2 + L^2*(\sin(ta1) - \sin(ta2))^2)^{(1/2)} / \\
& (2*L))) * (2*L^2*\sin(ta2)*(\cos(ta2) - \cos(ta1) + 2) + 2*L^2*\cos(ta2)*(\sin(ta1) - \\
& \sin(ta2)))) / (8*(L^2*(\cos(ta2) - \cos(ta1) + 2)^2 + L^2*(\sin(ta1) - \\
& \sin(ta2))^2)^{(1/2)} * (1 - (L^2*(\cos(ta2) - \cos(ta1) + 2)^2 + L^2*(\sin(ta1) - \\
& \sin(ta2))^2)/(4*L^2))^{(1/2)}) + (L^2*\text{M}*\sin(ta2)^2)/4 + (\text{Jp}*(2*L^2*\sin(ta2)*(\cos(ta2)
\end{aligned}$$

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- cos(ta1) + 2) + 2*L^2*cos(ta2)*(sin(ta1) - sin(ta2)))^2)/(8*L^2*conj((1 -
(L^2*(cos(ta2) - cos(ta1) + 2)^2 + L^2*(sin(ta1) - sin(ta2))^2)/
(4*L^2))^(1/2))*(L^2*(cos(ta2) - cos(ta1) + 2)^2 + L^2*(sin(ta1) - sin(ta2))^2)*(1 -
(L^2*(cos(ta2) - cos(ta1) + 2)^2 + L^2*(sin(ta1) - sin(ta2))^2)/(4*L^2))^(1/2)) +
(M*cos(angle(L*(sin(ta1) - sin(ta2))*(- 1 - 1i)) + acos((L^2*(cos(ta2) - cos(ta1) +
2)^2 + L^2*(sin(ta1) - sin(ta2))^2)^(1/2)/(2*L)))*cos(conj(acos((L^2*(cos(ta2) -
cos(ta1) + 2)^2 + L^2*(sin(ta1) - sin(ta2))^2)^(1/2)/(2*L))) + angle(L*(sin(ta1) -
sin(ta2))*(- 1 - 1i))))*(2*L^2*sin(ta2)*(cos(ta2) - cos(ta1) + 2) +
2*L^2*cos(ta2)*(sin(ta1) - sin(ta2)))^2)/(64*conj((1 - (L^2*(cos(ta2) - cos(ta1) +
2)^2 + L^2*(sin(ta1) - sin(ta2))^2)/(4*L^2))^(1/2))*(L^2*(cos(ta2) - cos(ta1) + 2)^2
+ L^2*(sin(ta1) - sin(ta2))^2)*(1 - (L^2*(cos(ta2) - cos(ta1) + 2)^2 + L^2*(sin(ta1)
- sin(ta2))^2)/(4*L^2))^(1/2)) + (M*sin(angle(L*(sin(ta1) - sin(ta2))*(- 1 - 1i)) +
acos((L^2*(cos(ta2) - cos(ta1) + 2)^2 + L^2*(sin(ta1) - sin(ta2))^2)^(1/2)/
(2*L)))*sin(conj(acos((L^2*(cos(ta2) - cos(ta1) + 2)^2 + L^2*(sin(ta1) -
sin(ta2))^2)^(1/2)/(2*L))) + angle(L*(sin(ta1) - sin(ta2))*(- 1 -
1i))))*(2*L^2*sin(ta2)*(cos(ta2) - cos(ta1) + 2) + 2*L^2*cos(ta2)*(sin(ta1) -
sin(ta2)))^2)/(64*conj((1 - (L^2*(cos(ta2) - cos(ta1) + 2)^2 + L^2*(sin(ta1) -
sin(ta2))^2)/(4*L^2))^(1/2))*(L^2*(cos(ta2) - cos(ta1) + 2)^2 + L^2*(sin(ta1) -
sin(ta2))^2)*(1 - (L^2*(cos(ta2) - cos(ta1) + 2)^2 + L^2*(sin(ta1) - sin(ta2))^2)/
(4*L^2))^(1/2)));

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